



HYDROGEN GAS PRODUCTION FROM GLYCEROL VIA STEAM REFORMING USING NICKEL LOADED ZEOLITE CATALYST

(Penghasilan Gas Hidrogen daripada Gliserol melalui Kaedah Pembaharuan Stim dengan menggunakan Pemangkin Nikel-Zeolite)

Fazureen Azaman¹, Hafizan Juahir^{1*}, Mahadhir Mohamed², Azman Azid¹, Kamaruzzaman Yunus³, Anis Farhana Abdul Rahman², Wan Nur Anis Amira Wan Ranizang², Fara Aiza Md Sanin², Mohammad Azizi Amran¹, Mohd Zaid Arqam Zainal Abidin¹, Norsyuhada Hairoma¹, Nur Hishaam Sulaiman¹, Ismail Zainal Abidin¹

¹East Coast Environmental Research Institute (ESERI),

Universiti Sultan Zainal Abidin, Gong Badak Campus, 21300 Kuala Terengganu, Terengganu, Malaysia

²Department of Chemical Engineering, Faculty of Chemical Engineering,

Universiti Teknologi Malaysia, 81310 UTM Skudai, Johor, Malaysia

³Kulliyah of Science,

International Islamic University Malaysia, 25200 Kuantan, Pahang, Malaysia

*Corresponding author: hafizanjuahir@unisza.edu.my

Received: 14 April 2015; Accepted: 9 July 2015

Abstract

Glycerol is the main by-product of biodiesel production that produces from transesterification process. In this research, focused was on hydrogen production via glycerol steam reforming using nickel loaded HZSM-5 catalyst. The catalysts were prepared by using different loading amount of nickel (0.5, 1.0, 5.0, 10.0 and 15 wt %) on HZSM-5 catalyst through the wet impregnation method at temperature 500 °C and atmospheric pressure. The catalyst was characterized by using XRD, FTIR and SEM. Then, only 15 wt % Ni loading has been chosen based on the parameter which is different range of catalyst weight (0.3-0.5g) at different range of glycerol flow rate (0.2-0.4mL/min) at temperature 600 °C and atmospheric pressure. The products were analyzed by using gas-chromatography with thermal conductivity detector (GC-TCD) where it is used to identify the yield of hydrogen. The data of the experiment were analyzed by using Response Surface Methodology (RSM) in order to study the relationship of catalyst weight and glycerol flow rate. The results showed that the optimum condition to produce a maximum hydrogen yield with 15wt% Ni/HZSM-5 catalyst was 78.10004% at glycerol flow rate of 0.356484 mL/min and catalyst weight of 0.429267 g.

Keywords: glycerol, transesterification, biodiesel, HZSM-5, hydrogen

Abstrak

Gliserol adalah produk sampingan utama penghasilan biodiesel yang terhasil daripada proses transesterifikasi. Dalam kajian ini, fokus utama adalah kepada penukaran gliserol terhadap gas hidrogen telah menggunakan HZSM-5 yang diubahsuai dengan nikel. Kajian ini dijalankan dengan menggunakan pemangkin 0.5, 1.0, 5.0, 10.0 and 15% nikel/ ZSM-5 pada tekanan atmosfera dan suhu 500 °C untuk penyediaan pemangkin. XRD, FTIR dan SEM digunakan untuk menganalisis struktur pemangkin. Kemudian, hanya 15 % nikel/ZSM-5 yang digunakan untuk menjalankan eksperimen seterusnya pada perbezaan berat pemangkin (0.3-0.5 g) dan kadar aliran gliserol (0.2-0.4 mL/min) pada tekanan atmosfera dan suhu 600 °C. Produk ini akan dianalisis dengan menggunakan kromatografi gas (GC-TCD) untuk mengkaji peratus hydrogen terhasil. Keputusan eksperimen menunjukkan 78.10004% penghasilan optimum gas hidrogen oleh 15% Ni/HZSM-5 pada keadaan optimum iaitu pada kadar aliran gliserol = 0.356484 mL/min and berat pemangkin = 0.429267 g.

Kata Kunci: gliserol, transesterifikasi, biodiesel, HZSM-5, hidrogen

Introduction

Glycerol is a by-product during manufacturing several chemicals such as petroleum, soap and biodiesel. Biodiesel is an alternative fuel for diesel engines that is produced from vegetable oil or animal fat with a simple monohydric alcohol such as methanol. The reaction requires a catalyst, usually a strong base, such as sodium hydroxide, and produces new chemical compounds called methyl esters. It is these esters that have come to be known as biodiesel. "The mono alkyl esters of long fatty acids derived from renewable lipid feedstock such as animal fats or vegetable oil, for use in compression ignition diesel engines" [1]. In simple terms, biodiesel is a renewable fuel manufactured from vegetable oil, methanol, animal fats, and also recycled cooking fats [2].

In general, biodiesel is produced through a process known as transesterification which involves altering the chemical properties of the oil by using methanol. Transesterification of plant oils with methanol is a simple process that gives high conversions of yields with only glycerol as a by-product. Glycerol production increased as the production of biodiesel increased due to the crude glycerol as a by-product of biodiesel production. The generation of crude glycerol gives a yield at about 10% (wt/wt) of biodiesel during the process of biodiesel production. In that case, by through the several of the analysis, the global biodiesel market is estimated to reach 37 billion gallons by 2016 with an average annual growth of 42%, that means about 4 billion gallons of crude glycerol will be produced [3].

Therefore, it is imperative to find alternative uses for glycerol. Glycerol has many uses in different industries, such as food, paint, pharmaceutical, cosmetic, soap, toothpaste and others. Besides, glycerol also can produce value-added chemicals by conversion of glycerol such as citric acid, lactic acid, hydrogen, ethanol and others [3]. The simplest and most abundant element is hydrogen, which is growing from time to time due to the technological advancements in fuel cell industry. Nowadays, almost 95% of hydrogen is produced from fossil fuel. Fossil fuels are not renewable resources. So, renewable resources based technologies for production of hydrogen are attractive options for the future due to the carbon neutral nature of these technologies with minor effects to the environment. We also have seen over the last few years, a great interest in utilizing glycerol for the production of hydrogen [4].

Hydrogen can be produced from glycerol by undergoing some processes such as steam reforming, autothermal reforming, aqueous-phase reforming and supercritical water reforming by Adhikari et al. [4] and they found that the best conditions for steam reforming to produce hydrogen is temperature above 627 °C, 9:1 of the molar ratio of water/glycerol and at atmospheric pressure. While, Adhikari et al. [5] Ni/CeO₂ was the best performing catalyst compared to the Ni/MgO and Ni/TiO₂ in terms of H₂ selectivity and glycerol conversion under the experimental conditions investigated. Ni/CeO₂ gave 74.7 % of H₂ selectivity which is maximum H₂ selectivity compared to the Ni/MgO (38.6%) and Ni/TiO₂ (28.3%) at a water/glycerol molar ratio (WGMR) of 12:1, 600 °C and 0.5 mL/min of feed flow rate.

Besides, Iriondo et al. [6] studied that the noble metals are active and stable for steam reforming, but the cost is quite high. For that reason, the non-noble metals such as nickel (Ni) and copper (Cu) are decided to be used as metal catalysts in this study due to the lower cost and more available than noble metals [7]. In addition, Nichele et al. [7] study has investigated that the best result for hydrogen production via glycerol steam reforming is achieved with Ni/ZrO₂ at 650 °C where hydrogen yield is 65% and glycerol conversion is 72%. Other study, Buhari [8] reported that 15wt% Ni-ZSM-5 has shown the best performance on hydrogen composition in product which 58.37% at temperature 600 °C. In this research, the objectives is to determine the relationship of catalyst weight (range = 0.3-0.5g) and glycerol flow rate (range = 0.2-0.4mL/min) at temperature 600 °C on 15wt% of the nickel loading by using the Response Surface Methodology (RSM) and to find the optimum condition for production of hydrogen gas.

Materials and Methods

Catalyst Preparation

HZSM-5 and nickel (II) nitrate hexahydrate was dissolved in 100 ml of distilled water. The mixed solution was stirred continuously overnight and dried in an oven overnight at 105 °C. Finally, the calcination process occurs where calcined in the furnace for 5 hours at 500 °C. The HZSM-5 zeolite catalyst was impregnated with nickel metals in different percentages as shown in Table 1.

Table 1. The amount of catalyst with different mass percent of Ni loading

No. of sample	Sample type	Weight of Ni loading (g)	Weight of Ni(NO ₃) ₂ loading (g)	Weight of HZSM-5 (g)
1	ZSM-5 (parent)	-	-	12.00
2	0.5 wt% Ni, 99.5wt% ZSM-5	0.06	0.2973	11.94
3	1.0 wt%Ni, 99.0 wt% ZSM-5	0.12	0.5946	11.88
4	5.0 wt% Ni, 95.0 wt% ZSM-5	0.60	2.9728	11.40
5	10.0 wt% Ni, 90.0 wt% ZSM-5	1.20	5.9457	10.80
6	15.0 wt% Ni, 85.0 wt% ZSM-5	1.80	8.9185	10.20

Catalyst Characterization: X-ray Diffraction (XRD)

X-Ray Diffraction (XRD) method was used to allow more accurate and precise information about the behavior of the alloy formation for the metal catalyst loading on HZSM-5. In this research, the structure of the nickel loaded zeolite catalyst was determined by using XRD techniques. XRD pattern was obtained on a Siemens D5000 goniometer. The pattern applied to the samples was: Cu K α radiation ($\lambda= 1.54056$ nm) at 40 kV and 20 mA and scanning angle is ranged from 5° to 60° with scan-step of 0.05° per second.

Fourier Transform Infra-Red (FTIR)

The existence of impregnated metal in zeolite catalyst was analyzed by Fourier Transform Infra-Red (FTIR) analyzer. The IR was obtained on a Shimadzu 3000 FTIR spectrometer using the KBr wafer technique. The sample about 0.25 mg of modified catalyst powder was mixed with 300 mg of spectrograde KBr powder. Then, placed it on a die, pressed and pelletized using hydraulic press. The range of 4000-370 cm⁻¹ of IR spectra was recorded at room temperature.

Scanning Electron Microscopy (SEM)

Scanning Electron Microscopy (SEM) methods were used to allow more accurate and precise information about the behavior of Ni/ZSM-5 catalyst. In this research, PHILIPS XL 40 model of scanning electron microscopy was used. The operating condition for electron gun was at a voltage of 30 kV. All samples were gold coated in a sputter coating unit by Bio-Rad and the photographic techniques was used to record the micrographs. The images were captured at 500:2000 magnification.

Reactivity Test

The performance of the catalyst for glycerol conversion was tested using the quartz tube in a fixed bed reactor as shown in Figure 1. The modified catalyst was placed in the core of the reactor that supported by quartz wool. The modified catalyst was activated by packing between glass wool inside the reactor at 600 °C of studied temperature. Nitrogen gas was emerged in the reactor for about 10-50 mL/min. WGMR was introduced in the process at the range of studied flow rate (0.2-0.4mL/min). Then, the heating process of glycerol was carried out in the preheater at a temperature about 250 °C. The reactor was activated for 30 minutes at 600 °C of studied temperature. The production flows through the condenser where the liquid product was collected while gas products continuously flow into a silica bed to trap any moisture in the product. The production of gaseous was analyzed by gas chromatography with thermal conductivity detector (GC-TCD) and being illustrated using computer.

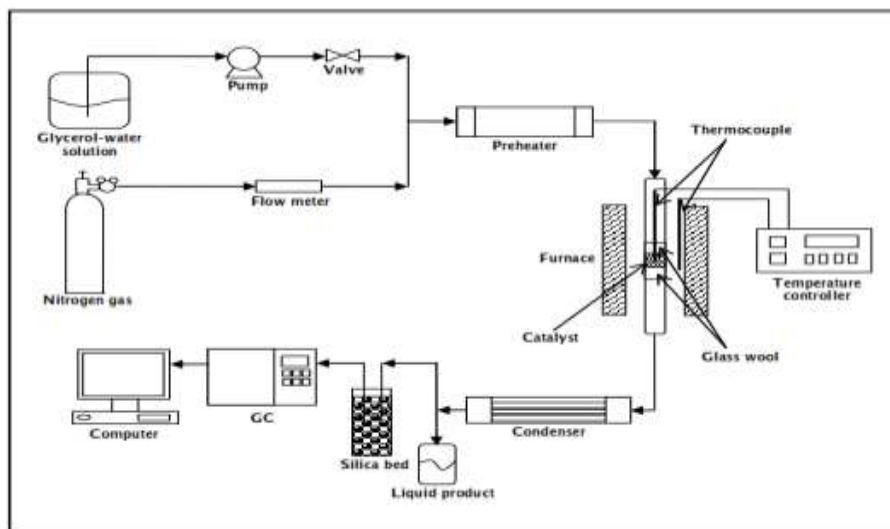


Figure 1. Schematic layout of the rig of the glycerol conversion

Response Surface Methodology (RSM)

Response surface methodology (RSM) was used to determine the relationship of glycerol flow rate and catalyst weight and also to optimize the reaction conditions. Kusworo et al. [9] proven that the RSM is successfully used to optimize the production of hydrogen from methane using fixed bed reactor process.

In this experiment, design of experiment (DOE) by using statistica was performed. The exact software of the statistica that used was Statsoft Statistica Release 7.0 software where their function is to determine the statistical analysis of hydrogen yield and glycerol conversion. By using the RSM in investigating the performance of (Ni/ZSM-5) catalyst, the central composite design (CCD) was used to predict the condition of optimum process for hydrogen yield and to study the interaction of process variables. The range and the coded level of the independent process variables studied are listed in Table 2. The process variables studied were catalyst weight (X_1) and glycerol flow rate (X_2). Each variable consisted of three different levels from low (-1) to medium (0) and to high (1).

Table 2. Experimental range and level coded of independent variables

Factors	Symbol	Range and levels		
		-1	0	+1
Catalyst weight, g	X_1	0.3	0.4	0.5
Glycerol flow rate, mL/min	X_2	0.2	0.3	0.4

The central composite design (CCD) that used in this research was 22 factorial designs, two central points and four star points. The total number of the experiment was 10 where 8 experiments with two replications at the central point to identify the errors.

Results and Discussion

Catalyst Characterization: X-ray Diffraction (XRD) Analysis

In this research, X-Ray Diffraction (XRD) was used to determine the structure of the nickel loaded zeolite catalyst and the present of crystalline phase. The analyses made with an angular range of 5° and 60° with scale 2θ . The diffraction samples were either powder (found by pestle milling) or cakes. Figure 2 shows the effect of XRD pattern for five differences of nickel loaded on zeolite catalyst. It can be seen that there were no changes on the modified catalyst based on the structure and the relative crystallinity of HZSM-5 after the modification. Jong-San Chang et al. [10] studied on the pentasil-type zeolite (ZSM-5) supported Ni catalysts and found that all the XRD patterns of supported nickel catalysts, which are not displayed or does not give the crystalline pentasil-type structure. Besides, from the observation on the XRD pattern, there were also observed of intensities differ between the metal contents. 15 wt % Ni loading on HZSM-5 gives highest intensity and followed by 10wt%, 5wt%, 1wt% and 0.5wt%. The intensity became decrease due to the high absorption coefficient of metals. Apart from that, the diffraction peaks at $2\theta = 37^\circ$ and 44.5° show that NiO was completely reduced to Ni. Apanee et al. [11] also studied on the activity of nickel loading on zeolite in his research and found that the crystalline of zeolite decreased slightly upon Ni incorporation. Other study, Na Shi et al. [12] showed that the nickel loading below 3wt%, there were no diffractions corresponding to NiO crystallite due to the small amounts of nickel loading dispersed highly on the support with very tiny particles. Nickel loading above 9wt% gave the diffraction intensity increased.

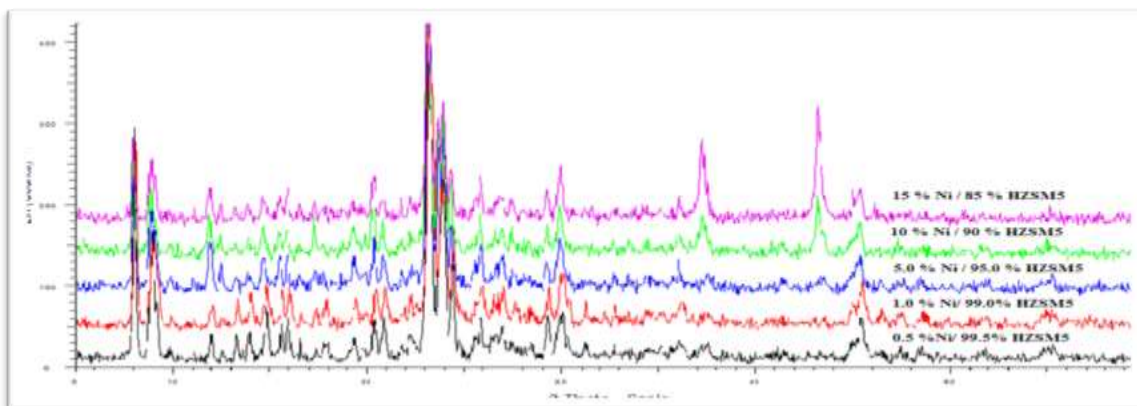


Figure 2. XRD pattern for 0.5%Ni 99.5%HZSM5, 1.0%Ni 99%HZSM5, 5%Ni 95%HZSM5, 10%Ni 90%HZSM5, and 15%Ni 85%HZSM

Fourier Transform Infra-Red (FTIR)

Fourier Transformed Infrared (FTIR) was used to analyze the existence of impregnated nickel in zeolite catalyst. Figure 3 shows the differences of mass percent of impregnated nickel in HZSM-5 catalysts. Based on the observation, the FTIR spectra shows that the impregnated nickel does not change the characteristic of zeolite catalyst. The broad band at $3600 - 3200 \text{ cm}^{-1}$ is attributed due to the stretching vibration of the bridging hydroxyl group associated with a framework of aluminium (Si-OH-Al) while the band at around 3440 cm^{-1} was assigned to the various OH groups associated with extra framework of Al. Besides, all the modified catalysts show the peak monitored at around 1635 cm^{-1} . There were also other four significant broad bands for all the modified catalysts which are at around 1080 cm^{-1} , 791 cm^{-1} , 545 cm^{-1} and 456 cm^{-1} compared with zeolite host were at 1636.19 cm^{-1} , 1102.81 cm^{-1} , 797.35 cm^{-1} , 547.71 cm^{-1} and 454.69 cm^{-1} . These results confirm the incorporation of Ni^{2+} cations into zeolite channels. Shams-Ghahfarokhi et al. [13] reported that the FT-IR spectrum of Ni-ZSM-5 shows a distortion of the spectrum between 1250 and 900 cm^{-1} . This region of the spectrum was assigned to asymmetrical T-O-T stretching and is indicative of heteroatom substitution. Changes of the characteristic peaks took place between the host zeolite ZSM-5 and the host-guest materials Ni-ZSM-5 and Ni-DMG/ZSM-5. For Ni-ZSM-5, the characteristic bands are seen at 456 cm^{-1} , 556 cm^{-1} (T-O bend), 791 cm^{-1} (symmetrical stretch), 1080 cm^{-1} (asymmetrical stretch), and 1235 cm^{-1} compared with ZSM-5 host were at around 446 cm^{-1} , 547 cm^{-1} (T-O bend), 786 cm^{-1}

(symmetrical stretch), 1082 cm^{-1} (asymmetrical stretch), and 1260 cm^{-1} that show a shift of some bands. These results confirm the incorporation of Ni^{2+} cations into zeolite channels. Furthermore, the presence of the peaks at 2410 and 2960 cm^{-1} in the Ni-ZSM-5 and Ni-DMG/ZSM-5 spectra, which are not present in the spectrum of ZSM-5, indicates the incorporation of Ni^{2+} into zeolite.

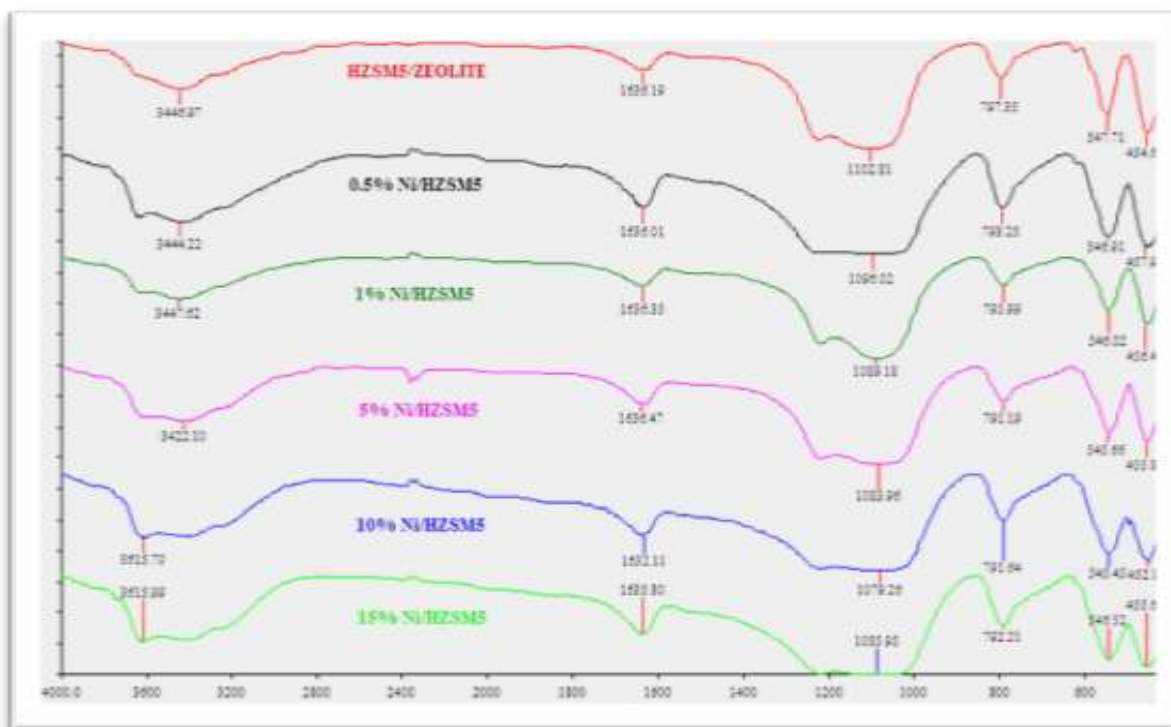


Figure 3. FTIR pattern for zeolite, 0.5%Ni 99.5%HZSM5, 1.0%Ni 99%HZSM5, 5%Ni 95%HZSM5, 10%Ni 90%HZSM5, and 15%Ni 85%HZSM

Scanning Electron Microscopy (SEM)

Scanning Electron Microscopy (SEM) was used to illustrate the images of differences of nickel loading on HZSM-5 as well as a parent of zeolite as shown in Figure 4. It is clearly seen that the crystal growth on large particles of zeolite is formed over all catalysts. Besides, from the SEM images also can be showed the influence of the impregnation of nickel on the zeolite. There was no transformation of crystalline occurred during the impregnation of nickel on zeolite due to the unchanged of nickel loaded on HZSM-5 catalyst respect to those parent of zeolite. Anne et al. [14] reported that there was only a small change on the micropore structure of the impregnation of nickel and cobalt on HY zeolite catalyst. This can be verified after impregnation, the micropore area and volume of all materials was decreased. Other study, Shams-Ghahfarokhi et al. [13] stated that Ni-ZSM-5 and Ni-DMG/ZSM-5) gave the crystallinity is not affected by the Ni^{2+} loading. But it seems that particles break into pieces with loading Ni^{2+} in the zeolite. Increasing activity of the loaded sample shows that the amount of small particle increased.

Catalyst Selection Performance

According to the studied methodology, there were five modified catalyst (0.5wt%, 1.0wt%, 5.0wt%, 10.0wt% and 15wt% of the nickel loading on HZSM-5) had been characterized to determine their performance of catalyst. In this research, only 15wt% of nickel loading was studied on the effect of catalyst weight and glycerol flow rate in order to achieve a higher percentage of hydrogen production. In this case, 15wt% had been selected due to the proven research done by Buhari [8] and reported that 15wt% Ni-ZSM-5 has shown the best performance on hydrogen

composition in product which 58.37%. Other study by Yun [15] stated that 5% Cu loaded on ZSM-5 was the only catalyst that could not obtained any of hydrogen yield. The addition of nickel into Cu/HZSM-5 catalyst had increased the hydrogen yield from 1.35 to 2.46 of mol H₂/mol C₃H₈O₃ (5wt% of Cu and 10wt% of Ni loaded on HZSM-5 catalyst) which was the highest hydrogen yield compared to 5wt% Cu, 5wt% Cu 0.5wt% Ni, 5wt% Cu 1.0wt% Ni, 5wt% Cu 5wt% Ni, 5wt% Ni, 5wt% Ni 0.5wt% Cu, 5wt% Ni 1.0wt% Cu and 5wt% Ni 5wt%. The investigation of different Ni content indicates that the Ni/CeO₂/ZSM-5 catalyst containing 2wt.% Ni showed poor catalytic activity in relation to the pyrolysis–gasification of polypropylene according to the theoretical potential H₂ production (7.2wt.%). Increasing the Ni loading to 5 or 10wt% in the Ni/CeO₂/ZSM-5 ((2-10)-5-500) catalyst, high potential hydrogen production was obtained [16]

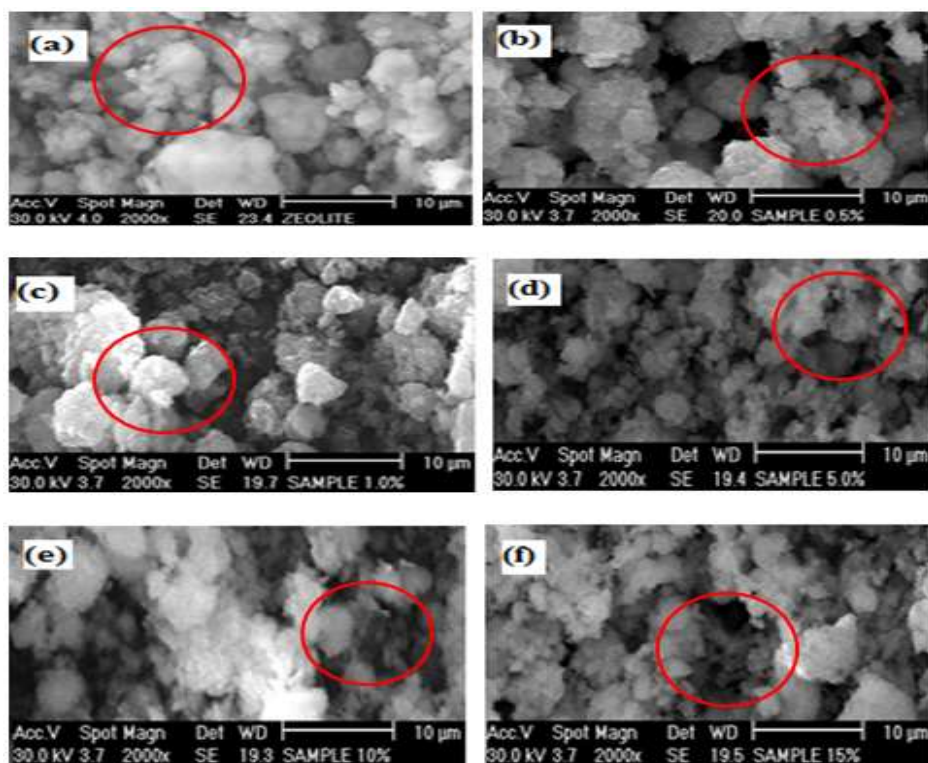


Figure 4. SEM pattern for (a) zeolite, (b) 0.5%Ni, 99.5%HZSM5 (c) 1.0%Ni, 99%HZSM5, (d) 5%Ni, 95%HZSM5, (e) 10%Ni, 90%HZSM5, (f) 15%Ni, 85%HZSM5

Response Surface Methodology Study

By using the response surface methodology (RSM) in investigating the performance of (Ni/ZSM-5) catalyst, the central composite design (CCD) was used to predict the condition of optimum process for hydrogen yield and to study the interaction of process variables. There were two independent variables which were catalyst weight and glycerol flow rate. Apart from that, RSM provides a design which gave a minimum number of experimental runs by using Statsoft Statistica Release 7.0 software. The experimental value and predicted response of hydrogen yield and glycerol conversion from statistical model for 10 runs were presented in Table 3 and Table 4 respectively.

Table 3. Experimental value and predicted response of hydrogen yield

Run	Variables		Hydrogen yield	
	Catalyst weight, X ₁ (g)	Glycerol flow rate, X ₂ (mL/min)	Experimental	Predicted
1	0.258579	0.300000	77.08704	69.72072
2	0.500000	0.200000	81.79643	83.38060
3	0.541421	0.300000	85.84106	89.94400
4	0.400000	0.300000	78.50265	78.50265
5	0.400000	0.300000	78.50265	78.50265
6	0.400000	0.441421	77.65270	81.68843
7	0.500000	0.400000	84.06105	77.63027
8	0.300000	0.400000	88.34577	90.02499
9	0.400000	0.158579	59.36768	52.06857
10	0.300000	0.200000	32.69169	42.38585

Table 4. Experimental value and predicted response of glycerol conversion

Run	Variables		Glycerol Conversion	
	Catalyst weight, X ₁ (g)	Glycerol flow rate, X ₂ (mL/min)	Experimental	Predicted
1	0.258579	0.300000	100	99.9696
2	0.500000	0.200000	100	100.0976
3	0.541421	0.300000	100	99.8954
4	0.400000	0.300000	100	100.0000
5	0.400000	0.300000	100	100.0000
6	0.400000	0.441421	99.61	99.5479
7	0.500000	0.400000	99.32	99.4099
8	0.300000	0.400000	100	100.0374
9	0.400000	0.158579	99.78	99.7071
10	0.300000	0.200000	99.53	99.5751

The relationship between the independent variables and response variables was estimated using regression analysis of the experimental data. Equation 1 presented a quadratic model for predicting the optimal point for the hydrogen yield.

$$Y_1 = 94.6077 + 11.0625X_1 + 22.1120X_2 - 28.7500X_1X_2 - 3.3750X_{12} - 18.6250X_{22} \quad (1)$$

The regression equation (Eq. 2) obtained for the glycerol conversion.

$$Y_2 = -183.35 + 418.73X_1 + 987.34X_2 - 1334.74X_1X_2 + 66.49X_{12} - 581.21X_{22} \quad (2)$$

where Y₁ and Y₂ are the response variables corresponding to the hydrogen yield and glycerol conversion respectively, while X₁ and X₂ represent the catalyst weight and the glycerol flow rate respectively, as independent variables.

Analysis of Variance (ANOVA) Responses

The analysis of variance (ANOVA) with a 5 % level of significance was used to test the empirical model for hydrogen yield and glycerol conversion as well as demonstrated the total, error and regression of sum of squares. The total, error and regression of sum of squares for hydrogen yield and glycerol conversion as shown in Table 5.

Table 5. Analysis of variance (ANOVA) for quadratic model

Sources	Sum of squares (SS)	Degree of freedom (d.f)	Mean squares (MS)	F-value	F _{0.05}
Hydrogen yield model					
Regression (SSR)	2209.119	5	441.8238	6.28211	6.26
Residual	281.322	4	70.3305		
Total (SST)	2490.441	9			
Glycerol conversion model					
Regression (SSR)	0.531962	5	0.106392	10.113308	6.26
Residual	0.042078	4	0.010520		
Total (SST)	0.574040	9			

From the table, the F-value indicates a ratio between the mean square of regression and mean square of error. Generally, the model is the best predictor of the experimental results with high confidence level of 95 % if the calculated F value greater than the tabulated F value. Therefore, the statistical model of the hydrogen yield in this research which 6.28211 was greater than $F_{0.05} = 6.26$. While, for the glycerol conversion, the calculated F value was 10.113308 greater than $F_{0.05} = 6.26$. Both of statistical models of hydrogen yield and glycerol conversion showed a good prediction model.

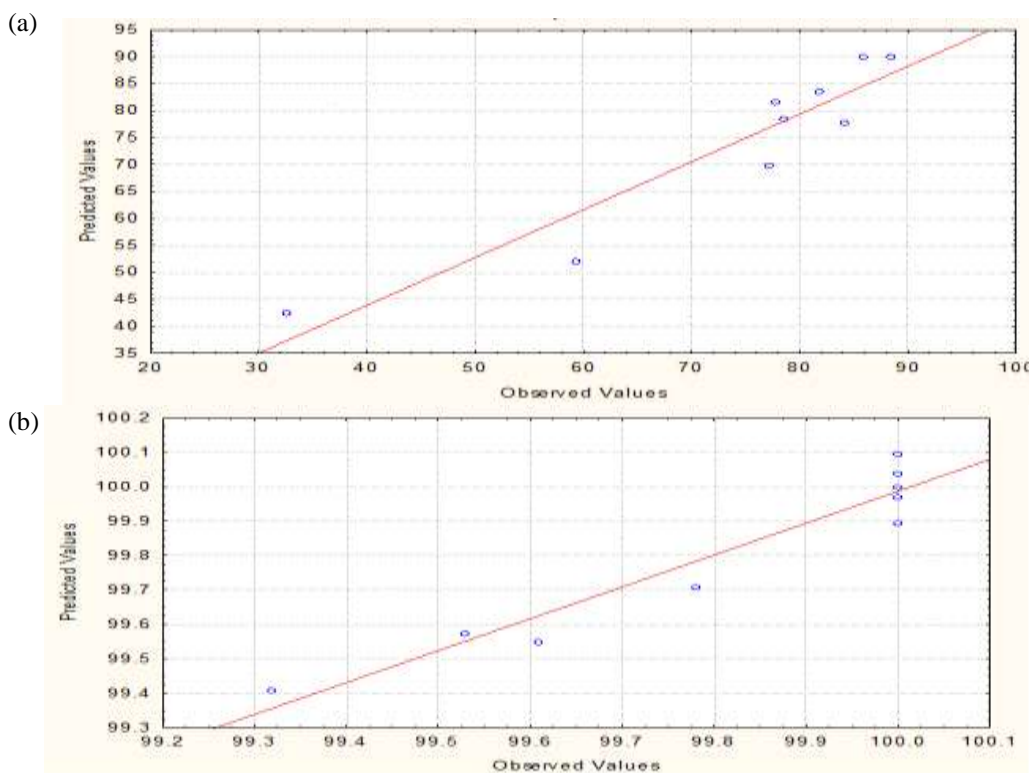


Figure 5. Parity plot for a) hydrogen yield and b) conversion

Besides, the comparison between the observed value and predicted value of hydrogen yield and glycerol conversion were shown in the Figure 5. The result indicates that the coefficient of determination (R^2) value for hydrogen yield is 0.88704 means 88.704 % of the variation of data can be explained by the model. Meanwhile, the R^2 value of the glycerol conversion is 0.92670 which 92.67 % indicating of the variation of data can be accounted to the model. The empirical model should be at least 0.75 to adequately explain most of the variability in the assay reading [17].

Another way to show the importance effects of variables is by using Pareto charts. In Pareto charts, factors are arranged from most significant to less significant and also considers whether the significance of the effect is at 95% confidence level. Figure 6 illustrates the Pareto chart and the corresponding p-values of the variables for hydrogen yield and glycerol conversion.

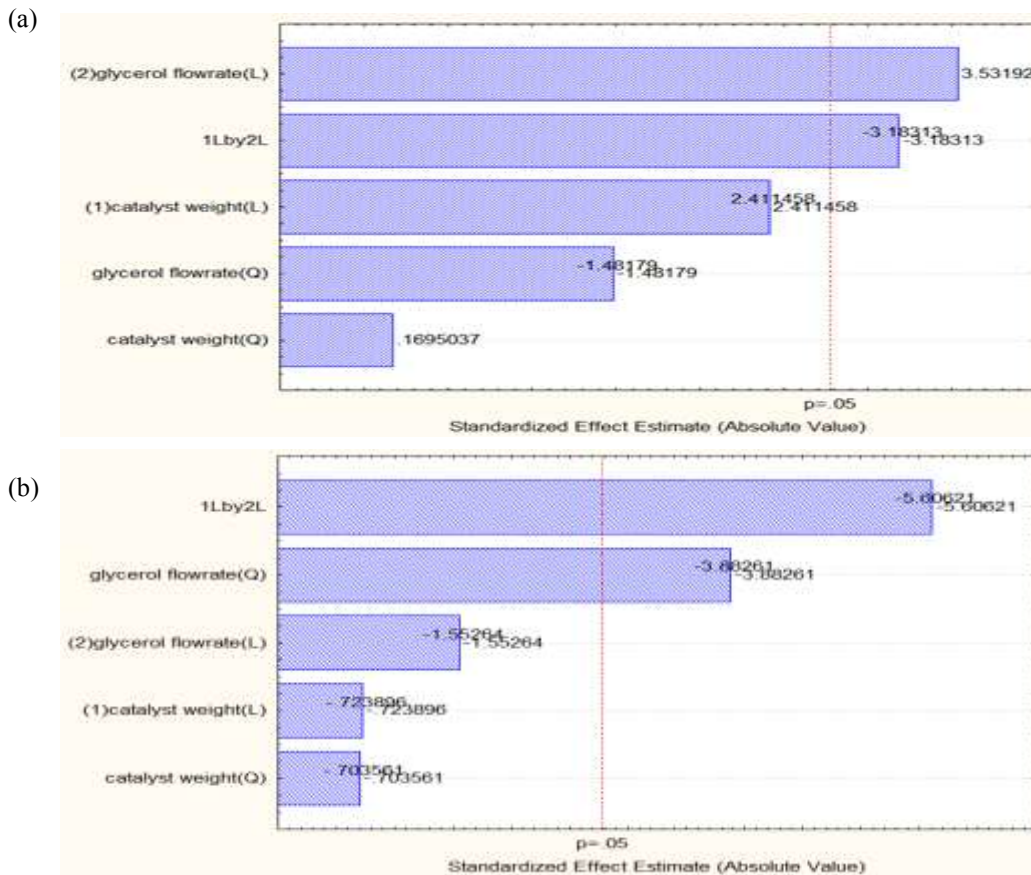


Figure 6. Pareto charts for (a) hydrogen yield and (b) glycerol conversion.

From the Pareto chart for hydrogen yield, glycerol flow rate (linear) gave the most significance, followed by interaction between catalyst weight (linear) and glycerol flow rate (linear). The catalyst weight (quadratic) was found to be insignificant towards hydrogen yield. Meanwhile, Pareto charts of effects show that the interaction between glycerol flow rate (linear) and catalyst weight (linear) gave the most significance towards glycerol conversion and followed by glycerol flow rate (quadratic). The most insignificant towards glycerol conversion was catalyst weight. Therefore, to determine the optimum hydrogen yield, the parameter of the glycerol flow rate was considered and for the glycerol conversion, the interaction between glycerol flow rate and catalyst weight was essential.

Interactive Effects of Variables on Hydrogen Yield and Glycerol Conversion

The interaction between variables in this study that gave impact to the hydrogen yield and glycerol flow rate was illustrated by using an empirical model which is plotted as three dimensional surfaces. Figure 7 depicts the effect of glycerol flow rate and catalyst weight interaction in the presence of 15 wt% of nickel loading and 600 °C on hydrogen yield and glycerol conversion, respectively. The interaction of these two variables indicated bigger impact on glycerol conversion. Meanwhile, the effect of glycerol flow rate gave the biggest impact to the hydrogen yield and followed by the interaction between glycerol flow rate and catalyst weight. As these were revealed in the Pareto chart and contour plot.

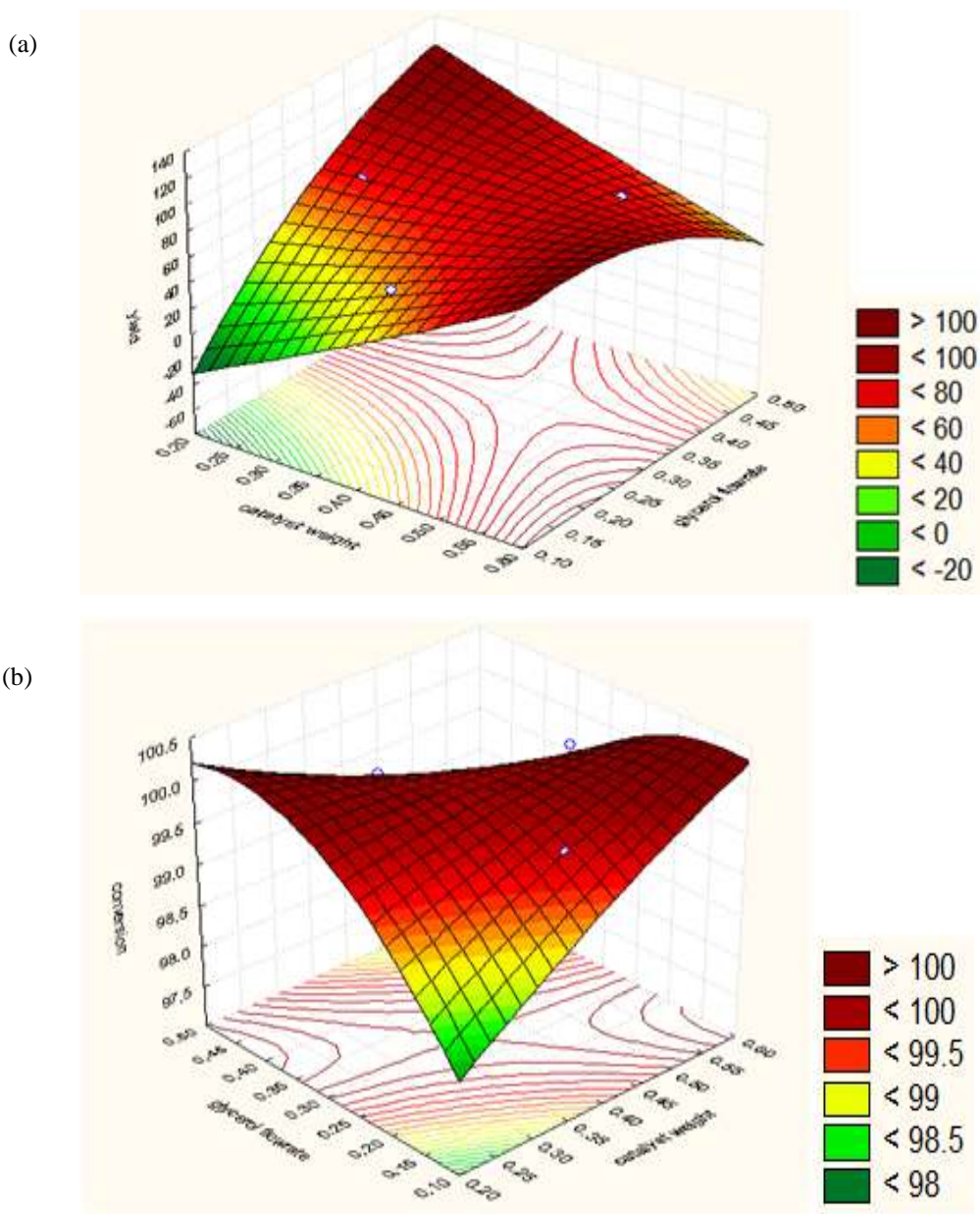


Figure 7. Response surface plot of the combination between glycerol flow rate and catalyst weight on (a) hydrogen yield and (b) glycerol conversion

Optimization of Hydrogen Yield

In this study, the optimum condition for hydrogen yield was obtained from the response surface methodology (RSM) by using Statsoft Statistica Release 7.0 Software. The response surface analysis indicated that the predicted optimum hydrogen yield of glycerol steam reforming.

Table 6. Optimum condition for predicted analysis of hydrogen yield

Factor	Observed minimum	Critical values	Observed maximum
Glycerol flow rate (mL/min)	0.158579	0.356484	0.441421
Catalyst weight (g)	0.258579	0.429267	0.541421

Hence, further experiment was performed to validate the optimization result obtained by the responses surface analysis at glycerol flow rate = 0.356484 mL/min and catalyst weight = 0.429267 as tabulated in Table 6.

Table 7. Comparison of optimum condition obtained from RSM between predicted and experimental of hydrogen yield

Responses	Observed value	Predicted value	Error (%)
Hydrogen yield (%)	78.10004	82.50653	5.07

Based on Table 7, the observed and predicted values for hydrogen yields are reported as 78.10004% and 82.50653%, respectively, where only 5.07% errors occurred. 5.07 % error occurs was considered small as the observed values are within 5 % level of significance. Hence, the result indicated that the statistical model is valid to use due to the small percentages of error. Therefore, the optimum condition for hydrogen yield were at glycerol flow rate = 0.356484 mL/min and catalyst weight = 0.429267 g.

Conclusion

The study showed that the optimum conditions to produce a maximum hydrogen yield (78.10004 %) of 15wt% of Ni/HZSM-5 in glycerol steam reforming were at glycerol flow rate of 0.356484 mL/min and catalyst weight of 0.429267 g. In addition, the interaction between glycerol flow rate and catalyst weight gave the largest effect on hydrogen yield and glycerol conversion.

Acknowledgement

The author would like to acknowledge to the East Coast Environmental Research Institute, Universiti Sultan Zainal Abidin and Faculty of Chemical Engineering, Universiti Teknologi Malaysia for the facilities.

References

1. Gerpen., J. V. (2005). Biodiesel Processing and Production. *Fuel Processing Technology* 86: 1097– 1107.
2. Shawn P. and Conley, B. T. (2006). What is Biodiesel? *BioEnergy*, ID337.
3. Xiaohu Fan, Burton, R. and Zhou, Y. (2010). Glycerol (Byproduct of Biodiesel Production) as a Source of Fuels and Chemicals-Mini Review. *The Open Fuels and Energy Science Journal* 3: 17-22.
4. Adhikari, S., Fernando, S. D. and Haryanto, A. (2009). Hydrogen Production from Glycerol: An update. *Energy Conversion and Management* 50: 2600-2604.
5. Adhikari S, Fernando S, To, F., Bricka R. M, Steele P. H. and Haryanto A. (2008). Conversion of Glycerol to Hydrogen via a Steam Reforming Process over Nickel Catalysts. *Energy Fuel* 22(2): 1220–1226.

6. Iriondo, A., Barrio, V. L., Cambra, J. F., Arias, P. L., Guemez, M. B., Navarro, R. M., Sanchez-Sanchez, M. C. and Fierro, J. L. G. (2009). Influence of La₂O₃ Modified Support and Ni and Pt Active Phases on Glycerol Steam Reforming to Produce Hydrogen. *Catalysis Communications* 10: 1275-1278.
7. Nichele, V., Signoretto, M., Menegazzo, F., Gallo, A., Santo, V. D., Cruciani, G. and Cerrato, G. (2012). Glycerol Steam Reforming for Hydrogen Production: Design of Ni Supported Catalysts. *Applied Catalysis B: Environment* 111: 225-232.
8. Buhari, J. (2013). Hydrogen Production from Glycerol using Nickel Loaded Zeolite Catalyst. *Degree Thesis*. Universiti Teknologi Malaysia.
9. Kusworo, T. D., Songip, A. R. and Amin, N. A. S. (2010). Optimization of Partial Oxidation of Methane for Hydrogen Production on NiO-CoO/MgO Catalyst using Design of Experiment. *IJET-IJENS*. 10(1): 1-8.
10. Jong-San Chang, S.-E. P., Kyu-Wan Lee, and Myoung Jae Choi (1994). Catalytic Reforming of Methane with Carbon Dioxide over Pentasil Zeolite-Supported Nickel Catalyst. *Studies in Surface Science and Catalysis*, 84: 1587-1594 .
11. Apanee, L. and Kaengsilalai, A. (2008). Activity of Different Zeolite-Supported Ni Catalyst for Methane Reforming with Carbon Dioxide. *Chemical Engineering Journal* 144: 96-102.
12. Na Shi, Q. L., Ting Jiang, T. W., Long, M., Qi Z. and Zhang, X., H. (2012). Hydrodeoxygenation of Vegetable Oils to Liquid Alkane Fuels over Ni/HZSM-5 Catalysts: Methyl Hexadecanoate as the Model Compound. *Catalysis Communications* 20: 80–84.
13. Nezamzadeh-Ejhieh, A. and Shams-Ghahfarokhi, Z. (2013). Photodegradation of Methyl Green by Nickel-Dimethylglyoxime/ZSM-5 Zeolite as a Heterogeneous Catalyst. *Journal of Chemistry*: 1-11.
14. Anne, M. G. P., Marcelo, J. B. S., Dulce, M. A. M. and Antonio. S. A. (2006). Cobalt and Nickel Supported on HY Zeolite: Synthesis, Characterization and Catalytic Properties. *Materials Research Bulletin* 41: 1105–1111.
15. Yun, H. B. A. H. (2013). Hydrogen Production from Glycerol Using Copper and Nickel Loaded Zeolite Based Catalyst. *Master Thesis*. Universiti Teknologi Malaysia.
16. Williams, C. W. P. T. (2009). Ni/CeO₂/ZSM-5 Catalysts for the Production of Hydrogen from the Pyrolysis–Gasification of Polypropylene. *International Journal of Hydrogen Energy* 15: 6242-6252.
17. Haaland, P. D. (1989). *Experimental Design in Biotechnology*. New York: Marcel Dekker Inc.
18. Slinn, M., Kendall, K., Mallon, C. and Andrews, J. (2008). Steam Reforming of Biodiesel By-Product to make Renewable Hydrogen. *Bioresource Technology* 99: 5851-5858.